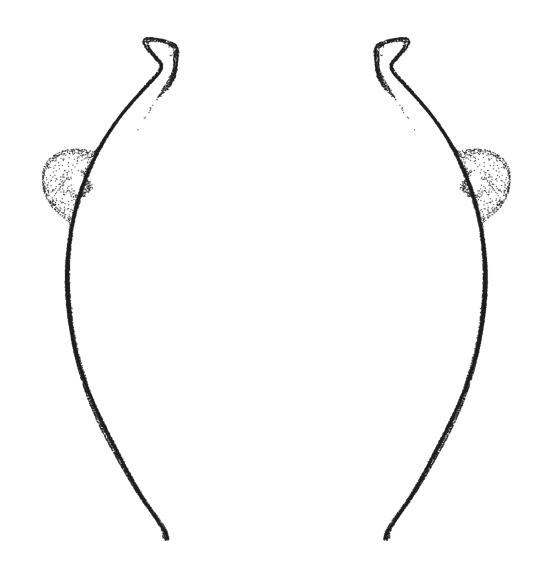
MV004 - Globular Ovoid Jar

An Exploration of Precision



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Petrie Museum, CC BY-NC-SA

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Artifact Information

Artifact Data

Collection Petrie Museum of Egyptian Archaeology

Provenance¹ Petrie Museum of Egyptian Archaeology (London), recovered by Flinders Petrie

Provenience² Unknown Attribution Naqada II

Museum information

Ref. LDUCE-UC15606

Description Basalt barrel vase, with two lug handles perforated horizontally, flat base, rim chipped.

URL https://collections.ucl.ac.uk/Details/collect/23647

Maijers vessel classification³

Short classification Globular Ovoid Jar

Long classification The vessel is created in a closed form classified as a globular jar with a ovoid shape, a

rounded rim.

Physical properties

Precision score⁴ 68

Height (approximate) 63 mm 2.48 in Width (approximate) 52 mm 2.05 in

Material Basalt
Mohs Hardness⁵ 5 - 7 (Basalt)

Weight

Scan information

Source Scanned by Artifact Foundation

Source file name UC15606_base_0.09.stl

Scan method Laser

Mesh decimation None, raw scan file used in the analysis

Number of vertices 1 892 086

¹The verifiable chain of custody of an artifact

²The location or site where an artifact was recovered

³Vessel artifact classification developed by W. Arnold Maijer and described in his publication Masters of Stone, ISBN 978-90-829212-0-5

⁴The precision score metric is described in Precision Score Of The Artifact, p. 40

⁵The Mohs scale is an ordinal scale, from 1 to 10, describing the materials resistance to abrasion (the ability of harder material to scratch softer material)

⁶Median distance between vertices

Alignment In The Cartesian Coordinate System

For precise and valid measurements of the vessel's geometry to be possible, the points of the scanned dataset must first and foremost be placed optimally in a Cartesian coordinate system. Several alignment methods and algorithms have been tested on a number of different vessels to determine the best way to achieve optimal alignment.

Any misalignment of the artifact will increase the error of the precision measurements, due to the distortion/ wobble effect caused by the misaligned object. To visualize this distortion, we can consider a representation of the three-dimensional point cloud data, folded to a two-dimensional plane. This folded representation is obtained by rotating all scanned points around an assumed center axis to y = 0, x > 0, thus resulting in a two-dimensional profile representation of all scanned vertices in the object.

Figure 1 illustrates this effect on a ideal ellipsoid. In the first image, the ellipsoid is perfectly aligned, resulting in a narrow and precise two-dimensional folded profile. As misalignments are introduced, the two-dimensional profile increases in width, visually showing the distortion, causing the error in the precision measurements to increase. While easy to understand visually, this distortion can also be objectively quantified, and as such used to compare the fitness of different assumed center axes against each other, and further to create an automated and solid process for optimal Cartesian alignment of the scan data.

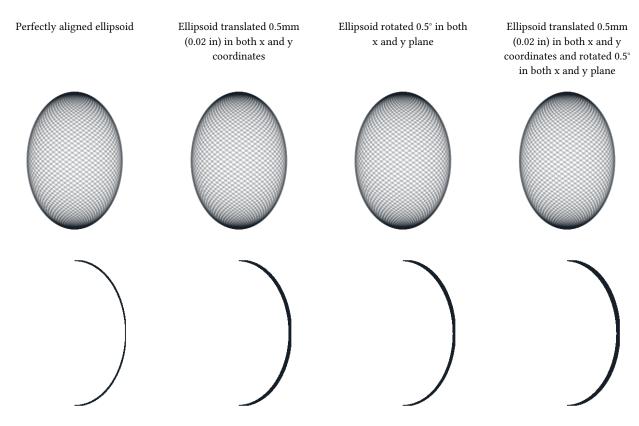


Figure 1: Distortion caused by a misalignment of the artifact

In contemporary metrology analysis of modern production objects, it is common to align the object in a Cartesian coordinate system by fitting a flat surface of the object to a reference plane in the coordinate system, cylindrical features to an ideal cylinder etc., or by using specific markers placed on the object in the design process. This methodology, however, is inadequate for the ancient objects in question. Most scanned artifacts, do not have a valid flat surface which could be aligned to a plane in the Cartesian coordinate system; most surfaces seem to be curved. Some artifacts do have a flat base, however this is often a worn area of the artifact and practical tests have shown that alignment to such surfaces will not produce optimal alignment of the scan data.

As conventional methods of alignment do not always yield good results with these types of artifacts, a more adequate method of alignment has been developed to enable precise measurements and statistical analysis of the scan data.

To find the optimal position of the vessel in the coordinate system, a range of rotation and translation tests are carried out to find the best fit of the central axis.

Based on the assumption that the analyzed object was created using a rotational process, and thus have symmetry around a central axis, the alignment of the artifact is carried out in a two-step process. An overview of this process is given below.

The artifact is placed in a Cartesian coordinate system, in an initially unaligned state. The first step in the alignment process estimates the central rotational axis of the vessel, by analyzing the coaxiality of thin cross-section slices of the vessel. The slices will be as thin as possible based on the mesh density of the scan, while still ensuring enough data points in each slice to be statistically valid.

For each slice, circular regression⁷ (estimate of best fit circle) is used to estimate the center point of this slice. Combined over the total Z-axis range of the vessel, these center points provide us with an indicator of the incline and position of the vessel's central axis.

The next step will optimize the center axis alignment by progressively minimizing the deviation (perpendicular to the surface curvature) of the two-dimensional profile, see Figure 1. By ascertaining and comparing the resulting fit of many thousands of different potential rotations, the best fit alignment of the scan data can be estimated, and an optimal center axis (in relation to the data points) can be reconstructed. The actual three-dimensional point-cloud is then aligned to this axis, by rotating and translating the scanned data points to match the Z-axis of the Cartesian coordinate system.

⁷Circle regression algorithm used: Kenichi Kanatani, Prasanna Rangarajan, "Hyper least squares fitting of circles and ellipses" Computational Statistics & Data Analysis, Vol. 55, pages 2197-2208, (2011)

Precision

To explore the manufacturing precision of the artifact in depth, the following analysis have been carried out:

- Circularity around the axis of symmetry is examined in detail at selected cross-sections.
- Overall circularity around the axis of symmetry is measured for the full height of the vessel (areas of the vessel with extensive damage are not taken into account for this metric).
- Concentricity of the vessel between selected cross-sections are examined in detail to determine if the existence of an axis of rotation in the manufacture of the object can be established.
- The coaxiality of the vessel is analyzed to explore the precision of the central axis of the object.
- The surface variability is analyzed and visualized on through a heatmap.

Circularity

Circularity is the measurement of how round the surface of an object is, optionally in reference to a datum axis. The *circularity tolerance* is the radial distance of two circles, each with their centers in the datum axis, and each of them conforming, respectively, to the minimum and maximum deviations of the data-set to a true circle, see Figure 2.

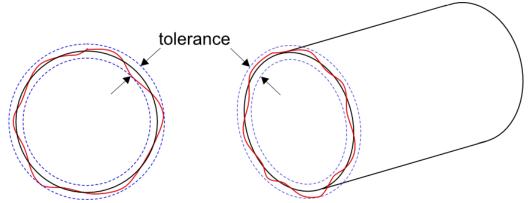


Figure 2: Circularity tolerance.

Circularity is examined at different cross-sections of the vessel, using the established Z-axis as the datum axis (axis of symmetry). The distance between the scanned points in the local datum plane is measured to determine the range between the two concentric circles encompassing the measured points, see Figure 3.

Referencing all of the individual circularity measurements to the global (reconstructed) axis of symmetry of the object, allows us to ascertain not only circularity of local features of the object, but how well circularity was *maintained* over the entire manufacturing process. This is an important distinction, which may be able to provide valuable insights into requirements of the construction methods. For reference, and seeing that the variance in local circularity also holds interest, measurements of circularity of the vessel without reference to the axis of symmetry can additionally be found in the Concentricity, p. 22.

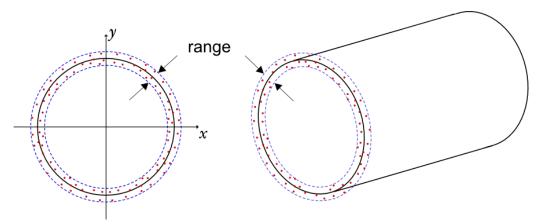


Figure 3: Circularity measurements.

If the circularity is determined from slices of the vessel exclusively in the *Z-plane* (actually measuring the cylindricity of a very thin slices of the vessel, in an attempt to approximate circularity), this would - in some areas - introduce significant distortion (increasing measurement errors) in the samples, due to the curvature of the vessel's surface.

Each sample slice of the vessel is therefore obtained perpendicular to the surface curvature, see Figure 5 to Figure 10. The measurements are taken conservatively without filtration of potential outliers.

To explore the potential distortion caused by obtaining samples in the Z-plane only, please refer to Appendix A, where measurements in the Z-plane and measurements perpendicular to surface curvature are compared side by side.

Detailed circularity measurements of selected points

Circularity measurements across a range of selected slices of the vessel (see Table 1) have been analyzed in-depth, and detailed plots of each measurement is provided. Furthermore, full circularity measurements are shown for each available scanned surface including a detailed plot to visualize the circularity of all areas of the vessel.

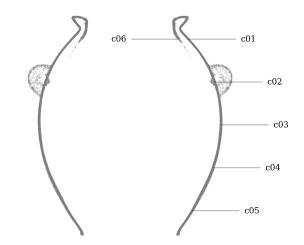


Figure 4: Circularity measurement sample location on MV004.

Metric

Tag	Area	Measured	Residuals	s			Sample	Slice	Slice		
		deviation ⁸	Range	RMSD ⁹	MAD ¹⁰	SD	size	Height	Z coord.	Radius11	
		mm	$_{ m mm}$	mm	mm	mm		mm	mm	$_{ m mm}$	
c01	exterior	Ø33.296±0.181	0.357	0.092	0.066	0.092	719	0.050	56.064	16.648	
c02	exterior	Ø48.363±0.262	0.486	0.102	0.068	0.102	1102	0.050	43.831	24.182	
c03	exterior	Ø51.991±0.343	0.594	0.139	0.110	0.139	1556	0.050	31.598	25.996	
c04	exterior	Ø47.310±0.339	0.621	0.134	0.072	0.134	1328	0.050	19.365	23.655	
c05	exterior	Ø35.338±0.292	0.497	0.120	0.080	0.120	912	0.050	7.133	17.669	
c06	interior	Ø27.897±0.312	0.609	0.160	0.134	0.153	222	0.050	56.064	13.949	

Imperial

Tag	Area	Measured	Residuals	s			Sample	Slice		
		deviation ⁸	Range	RMSD ⁹	MAD ¹⁰	SD	size	Height	Z coord.	Radius ¹¹
		in	in	in	in	in		in	in	in
c01	exterior	Ø1.3109±0.0071	0.0140	0.0036	0.0026	0.0036	719	0.0020	2.2072	0.6554
c02	exterior	Ø1.9041±0.0103	0.0191	0.0040	0.0027	0.0040	1102	0.0020	1.7256	0.9520
c03	exterior	Ø2.0469±0.0135	0.0234	0.0055	0.0043	0.0055	1556	0.0020	1.2440	1.0234
c04	exterior	Ø1.8626±0.0133	0.0245	0.0053	0.0028	0.0053	1328	0.0020	0.7624	0.9313
c05	exterior	Ø1.3912±0.0115	0.0196	0.0047	0.0032	0.0047	912	0.0020	0.2808	0.6956
c06	interior	Ø1.0983±0.0123	0.0240	0.0063	0.0053	0.0060	222	0.0020	2.2072	0.5492

Table 1: Detailed circularity measurements at selected samples of MV004.

Figure 5 to Figure 10 shows a detailed plots of each circularity measurement.

 $^{^8} Sample$ diameter ر maximum measured deviation from measured radius

⁹Root mean square deviation (RMSD) also called Root mean square error (RMSE)

¹⁰Median absolute deviation

 $^{^{\}scriptscriptstyle{11}}$ Median sample radius from z-axis

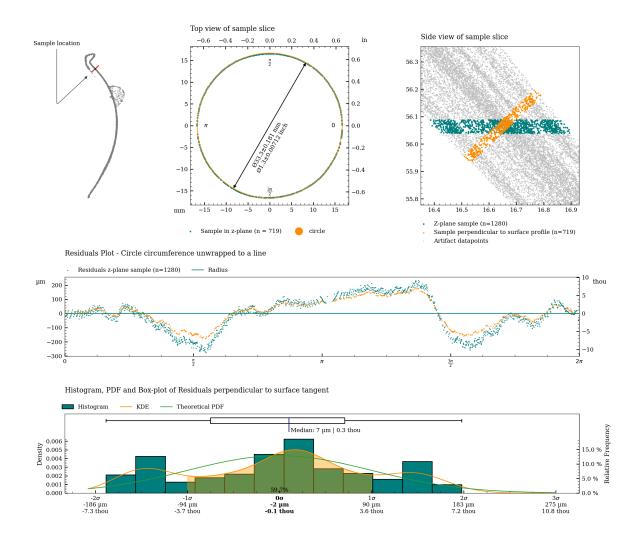


Figure 5: Charts with statistics for the measurement of c01.

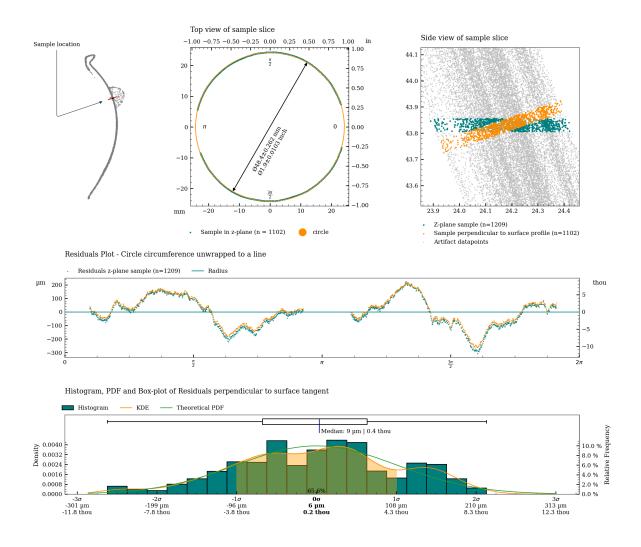


Figure 6: Charts with statistics for the measurement of c02.

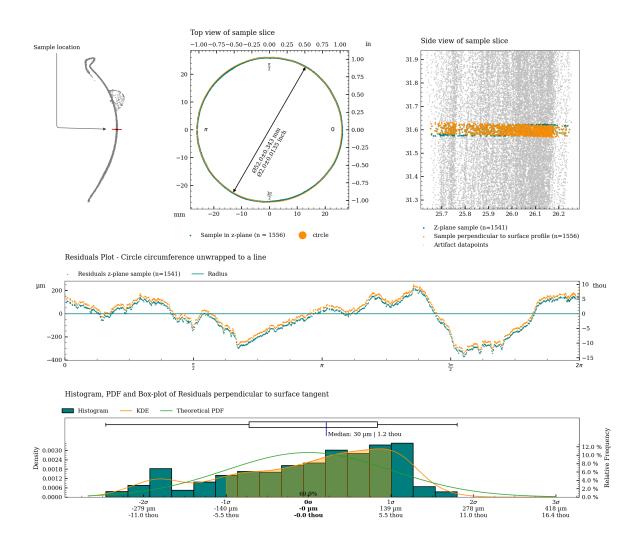


Figure 7: Charts with statistics for the measurement of c03.

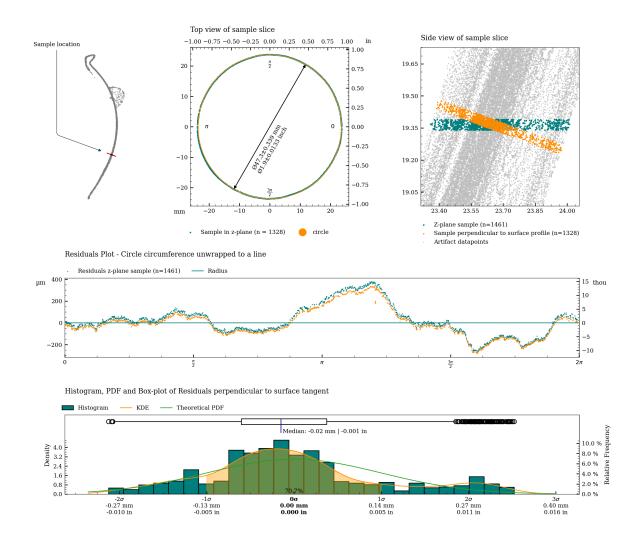


Figure 8: Charts with statistics for the measurement of c04.

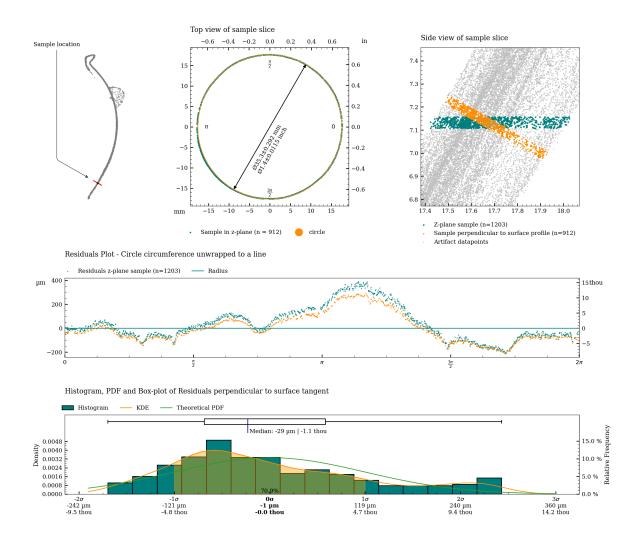


Figure 9: Charts with statistics for the measurement of c05.

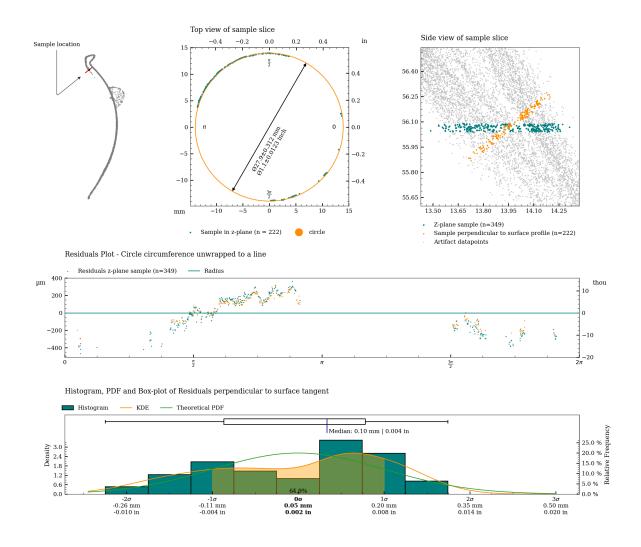


Figure 10: Charts with statistics for the measurement of c06.

Table 2 shows statistical measures of the circularity of the vessel, measured along the full height (damaged parts may reduce the measurement area).

Metric

Area	Range			Standard	Standard Deviation			solute Dev	Slices	Slice	
	Median	Min.	Max.	Median	Min.	Max.	Median	Min.	Max.		height
	$_{ m mm}$	$_{ m mm}$	$_{ m mm}$	mm	$_{ m mm}$	$_{ m mm}$	$_{ m mm}$	$_{ m mm}$	$_{ m mm}$		$_{ m mm}$
Exterior	0.524	0.294	0.762	0.115	0.079	0.182	0.009	0.046	0.120	1194	0.050
Interior	0.706	0.470	1.284	0.168	0.099	0.233	0.010	0.057	0.205	124	0.050

Imperial

Area	Range			Standard	Standard Deviation M			Medan Absolute Deviation			Slice
	Median	Min.	Max.	Median	Min.	Max.	Median	Min.	Max.		height
	in	in	in	in	in	in	in	in	in		in
Exterior	0.524	0.294	0.762	0.115	0.079	0.182	0.009	0.046	0.120	1194	0.050
Interior	0.706	0.470	1.284	0.168	0.099	0.233	0.010	0.057	0.205	124	0.050

Table 2: Perpendicular Circularity analysis of MV004.

Circularity analysis of exterior surface

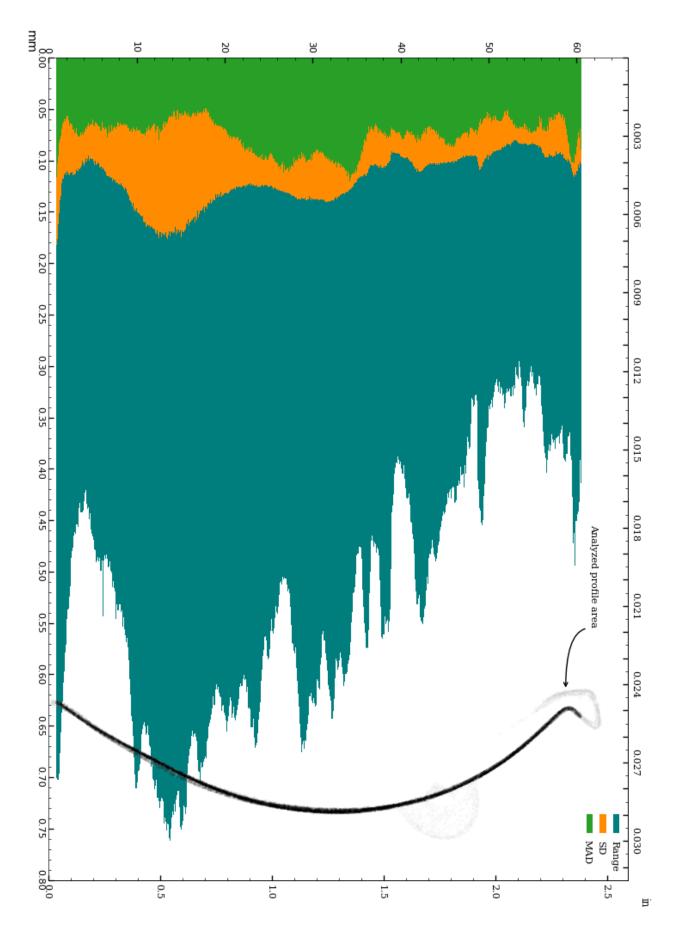


Figure 11: Circularity of exterior surface.

Circularity analysis of exterior surface, Standard Deviation and Median Absolute Deviation

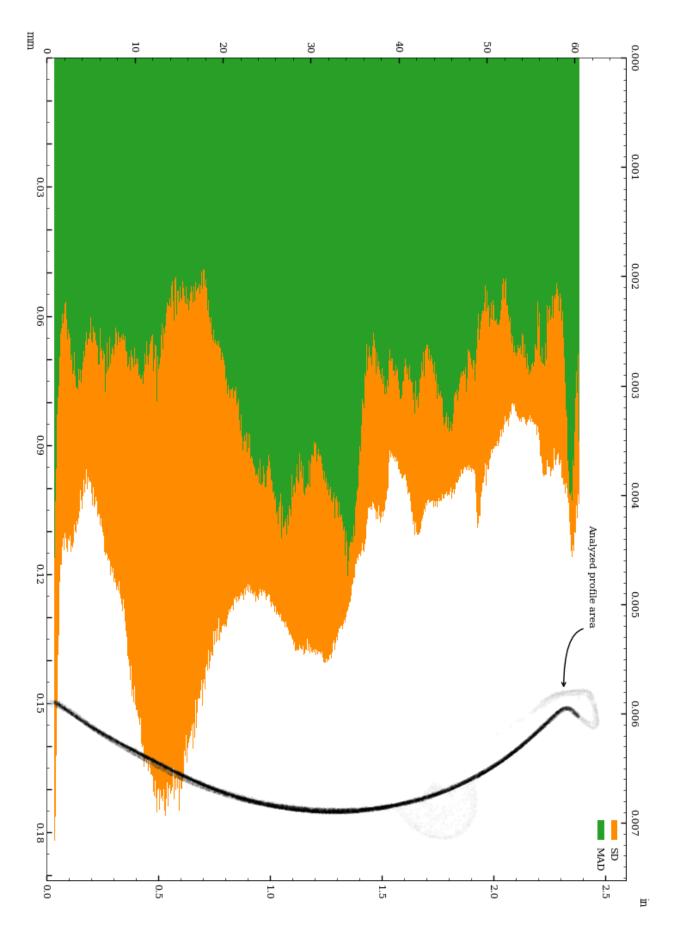


Figure 12: Vessel circularity of exterior surface, standard deviation and median absolute deviation.

The distributions of the circularity measurements across 1194 slices of the exterior surface are shown below.

Range measurement distribution across 1194 slices of exterior surface

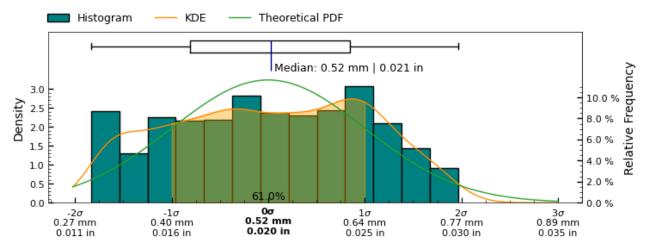


Figure 13: Range measurement distribution across measured slices of exterior surface

Standard deviation measurement distribution across 1194 slices of exterior surface

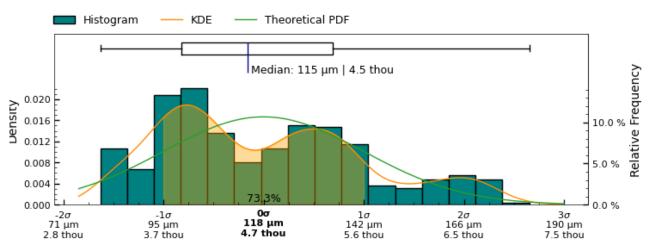


Figure 14: Standard deviation measurement distribution across measured slices of " + exterior + " surface

Median absolute deviation measurement distribution across 1194 slices of exterior surface

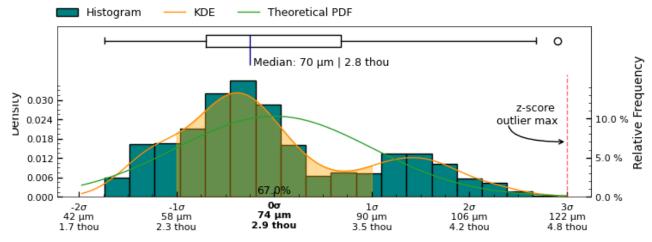


Figure 15: Median absolute deviation measurement distribution across measured slices of exterior surface

Circularity analysis of interior surface

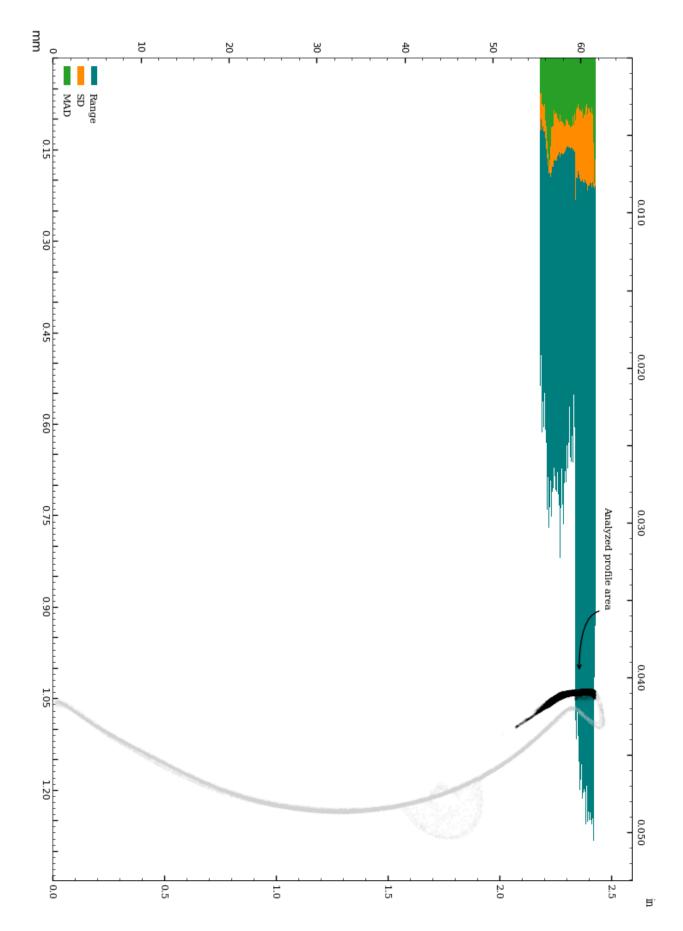
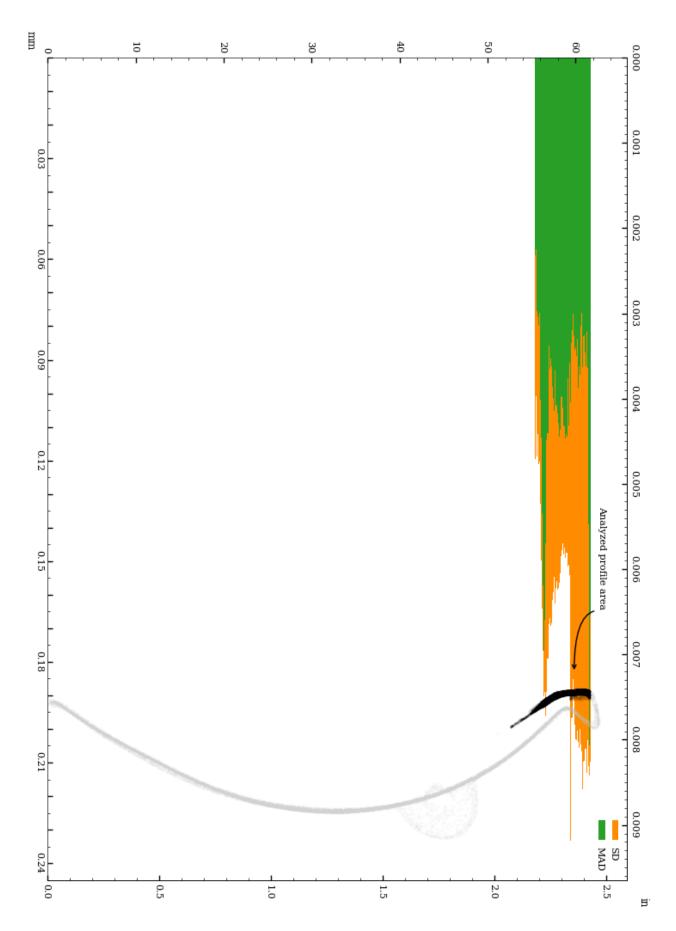


Figure 16: Circularity of interior surface.

Circularity analysis of interior surface, Standard Deviation and Median Absolute Deviation



 $Figure\ 17: Vessel\ circularity\ of\ interior\ surface,\ standard\ deviation\ and\ median\ absolute\ deviation.$

The distributions of the circularity measurements across 124 slices of the interior surface are shown below.

Range measurement distribution across 124 slices of interior surface

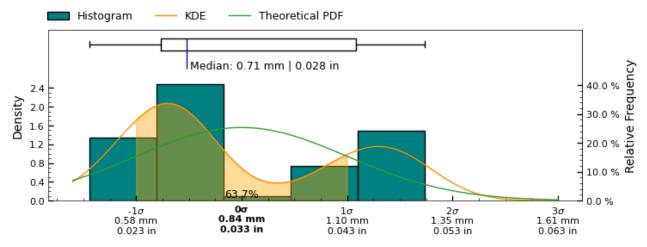


Figure 18: Range measurement distribution across measured slices of interior surface

Standard deviation measurement distribution across 124 slices of interior surface

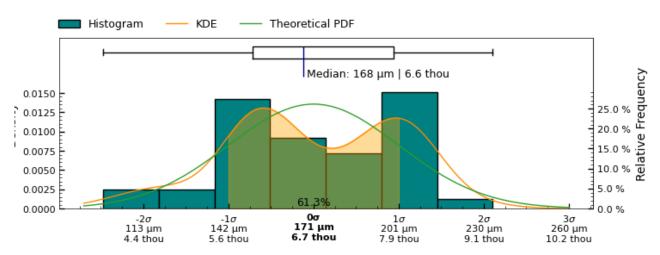


Figure 19: Standard deviation measurement distribution across measured slices of " + interior + " surface

Median absolute deviation measurement distribution across 124 slices of interior surface

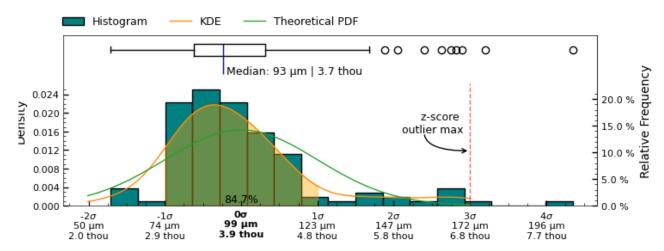


Figure 20: Median absolute deviation measurement distribution across measured slices of interior surface

Concentricity

The concentricity metric describes the deviation in the center-point of the referenced features. As such, it is a measure to determine if several features of the object share the same center point/axis, and how closely. See Figure 21 for a visual representation of this metric.

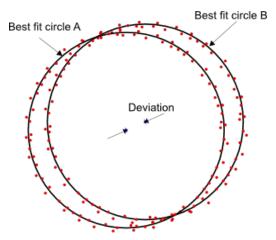


Figure 21: Concentricity measures the deviation (distance) between the center of two circles.

Determination of concentricity has been carried out by establishing the best fit circles of sample slices, using RANSAC (Random sample consensus) algorithm for outlier detection of a least squares circle regression on the scanned data-points at each cross-section, to estimate centers of each cross-section.

The concentricity between both the interior and exterior circular cross-sections is explored for cross-section measurements with the same Z-coordinates.

Additionally, the concentricity between each cross-section measurement defined in Figure 4 and the datum axis (x, y) = (0, 0) has been calculated to establish the deviation of the feature center from the datum axis.

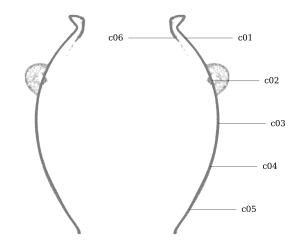


Figure 22: Concentricity measurement sample location on MV004.

Metric

Tag	Reference	Deviation	Sample	Circle fit residuals analysis for sample listed in Tag column						
			size	Range full	Range inliers	SD full	SD inliers	MAD full	MAD inliers	Center (x,y)
		$_{ m mm}$		$_{ m mm}$	$_{ m mm}$	$_{ m mm}$	$_{ m mm}$	$_{ m mm}$	$_{ m mm}$	$\mu \mathrm{m}$
c01	z-axis	0.046	706	0.357	0.357	0.093	0.093	0.062	0.062	-38, -26
c02	z-axis	0.018	1102	0.486	0.486	0.102	0.101	0.069	0.069	12, 13
c03	z-axis	0.020	1556	0.594	0.594	0.139	0.139	0.101	0.101	20, 1
c04	z-axis	0.095	1328	0.621	0.621	0.134	0.134	0.066	0.066	-95, 12
c05	z-axis	0.111	912	0.497	0.497	0.120	0.120	0.074	0.074	-110, 8
c06	z-axis	0.203	222	0.609	0.609	0.153	0.153	0.121	0.121	-202, 17
c01	c06	0.170	706	0.357	0.357	0.093	0.093	0.062	0.062	165, -43

Imperial

Tag	Reference	Deviation	Sample	Circle fit residuals analysis for sample listed in Tag column							
			size	Range full	Range inliers	SD full	SD inliers	MAD full	MAD inliers	Center (x,y)	
		in		in	in	in	in	in	in	thou	
c01	z-axis	0.0018	706	0.0140	0.0140	0.0037	0.0037	0.0024	0.0024	-1.5, -1.0	
c02	z-axis	0.0007	1102	0.0191	0.0191	0.0040	0.0040	0.0027	0.0027	0.5, 0.5	
c03	z-axis	0.0008	1556	0.0234	0.0234	0.0055	0.0055	0.0040	0.0040	0.8, 0.0	
c04	z-axis	0.0038	1328	0.0245	0.0245	0.0053	0.0053	0.0026	0.0026	-3.7, 0.5	
c05	z-axis	0.0044	912	0.0196	0.0196	0.0047	0.0047	0.0029	0.0029	-4.3, 0.3	
c06	z-axis	0.0080	222	0.0240	0.0240	0.0060	0.0060	0.0048	0.0048	-8.0, 0.7	
c01	c06	0.0067	706	0.0140	0.0140	0.0037	0.0037	0.0024	0.0024	6.5, -1.7	

Table 3: Concentricity analysis of MV004.

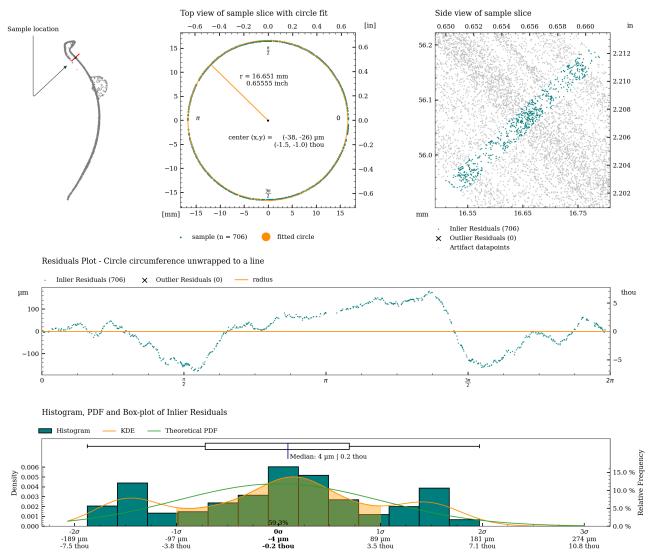


Figure 23: Detailed plot of concentricity measurement for c01.

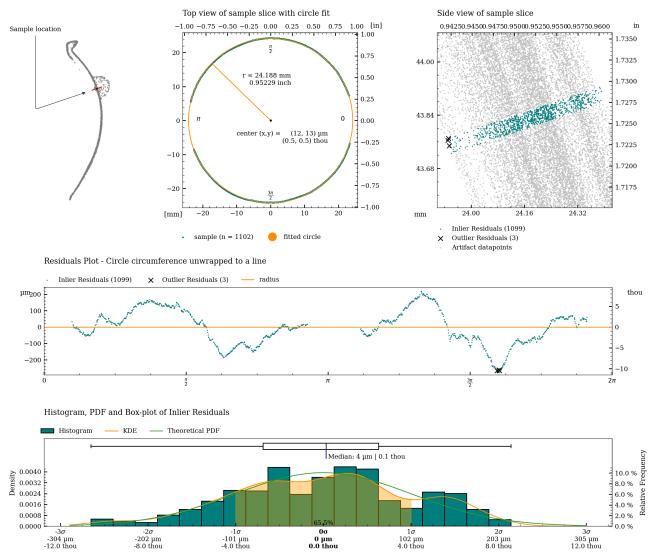


Figure 24: Detailed plot of concentricity measurement for c02.

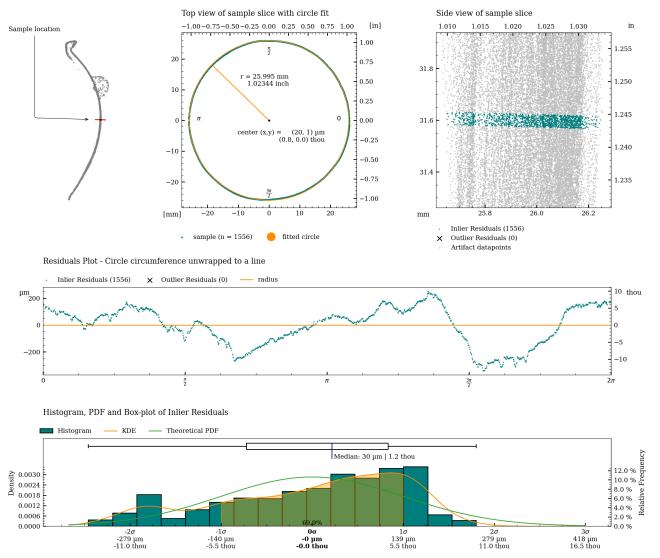


Figure 25: Detailed plot of concentricity measurement for c03.

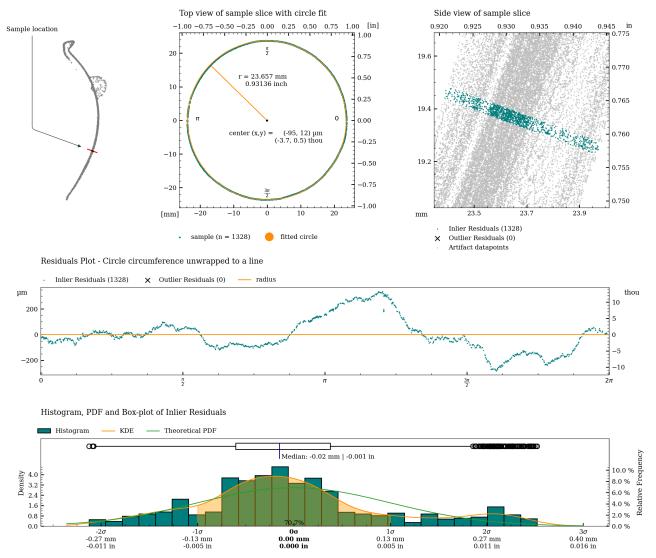


Figure 26: Detailed plot of concentricity measurement for c04.

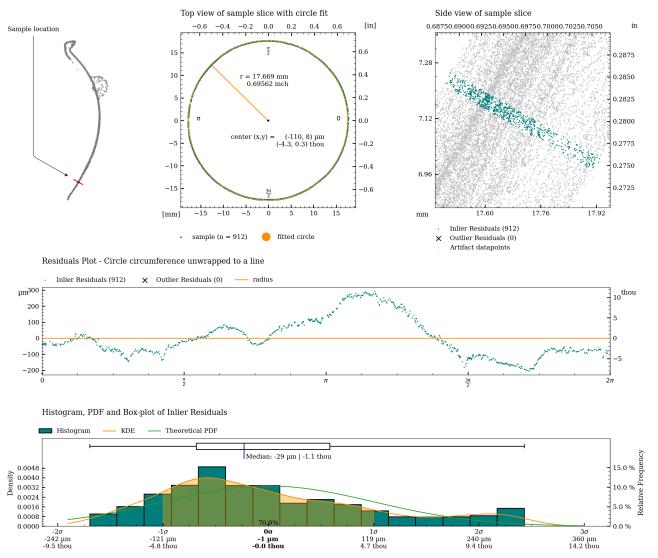


Figure 27: Detailed plot of concentricity measurement for c05.

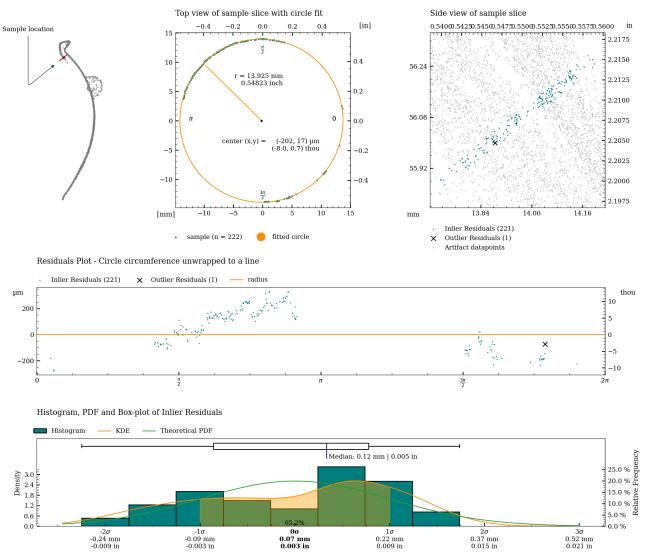


Figure 28: Detailed plot of concentricity measurement for c06.

Coaxiality

Coaxiality is a measure of the deviation in the central axis of an object. Coaxiality measurements are calculated using RANSAC (Random sample consensus) algorithm for outlier detection of a least squares circle regression on cross-sections of the vessel (excluding potential handles) to estimate the best fit circle centers for each slice of the vessel.

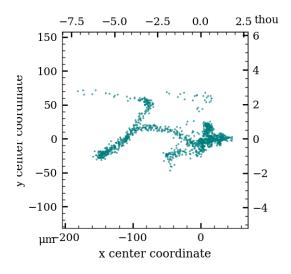
Coaxiality is measured for:

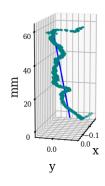
- The exterior surface (excluding handles)
- The interior surface

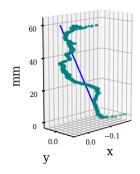
	Exterior	In	terior	
Analyzed Slices		1194		124
Median sample size		1104		720
Slice Height	50 μm	2.0 thou	50 μm	2.0 thou
Statistics with Z-axis as Reference				
Median Absolute Deviation (MAD)	32 μm	1.3 thou	199 μm	7.8 thou
Standard Deviation (SD)	48 μm	1.9 thou	34 μm	1.4 thou
Root Mean Square Deviation (RMSD)	74 μm	2.9 thou	197 μm	7.8 thou
Statistics with Best Fit Central Axis as Reference	ce			
Best fit Central Axis Equation	x = -0.116 + t0.00254	X =	-0.337 + t0.00285	
(in metric coordinate system with unit [mm])	y = 0.011 + t - 0.00026	y =	= -1.289 + t0.02340	
	z = 0.000 + t1.00000	z =	= 0.000 + t0.99972	
Axis tilt		0.145°		0.16°
Median Absolute Deviation (MAD)	40 μm	1.6 thou	35 μm	1.4 thou
Standard Deviation (SD)	22 μm	0.9 thou	21 μm	0.8 thou
Root Mean Square Deviation (RMSD)	46 μm	1.8 thou	44 μm	1.7 thou

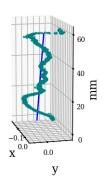
Table 4: Coaxiality analysis of vessel MV004.

Coaxiality plots, exterior surface









Coaxiality residuals from fitted axis, exterior surface

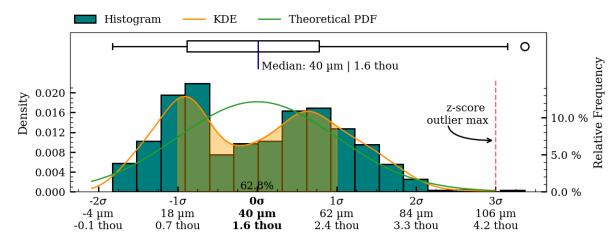
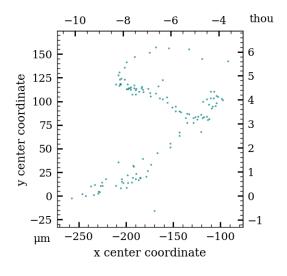
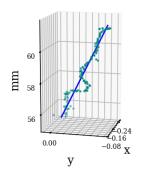
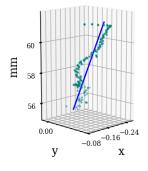


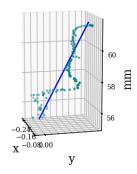
Figure 29: Coaxiality residual plots of exterior surface, MV004.

Coaxiality plots, interior surface









Coaxiality residuals from fitted axis, interior surface

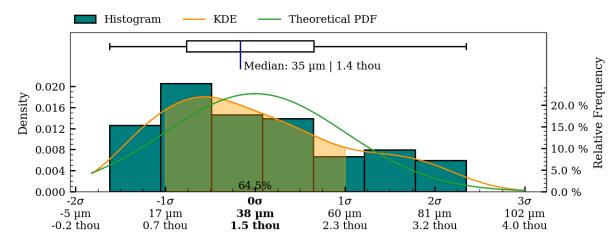


Figure 30: Coaxiality residual plots of interior surface, MV004.

Surface Variability

To illustrate the overall surface deviations of the object, a surface variability heatmap has been created. This heatmap provides an accessible overview of the topography of the manufacturing precision and surface structure of the object.

The surface variability measurements are created by fitting a number of higher-order polynomials to the twodimensional folded profile of the scan data. This process creates an idealized mathematical representation of actual surface curvature of object, and as such provides a continuous model representation of the actual object. It is important to note that only such a non-discretized representation is sufficient to avoid introducing inconsistently varying errors in the mapping of the final surface deviation results, that the rendered heatmaps are based on.

To produce the final surface variability map, the distance from each scanned vertex to the fitted polynomial is calculated and used as the mapping function input, for applying colours to the surface of the object.

It is important to note that this variability map does not describe deviations from the original *intended* shape of the artifact (if any), as this shape (the *intended design*, so to speak) will have been lost to time. It does however provide a very informative visualization of the texture and structure of the surface and very importantly, *does* hightlight potential manufacturing-relevant patterns in the surface texture (if present). Such patterns are, as an example, clearly evident on the interior surface of artifact PV001.

Exterior surface

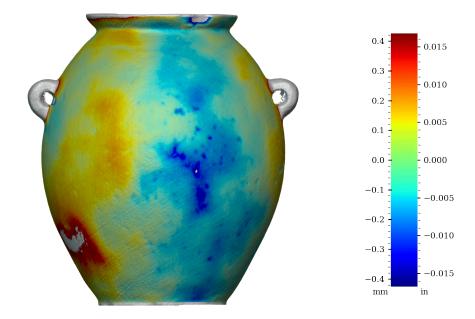


Figure 31: Surface variability heatmap of MV004, front view

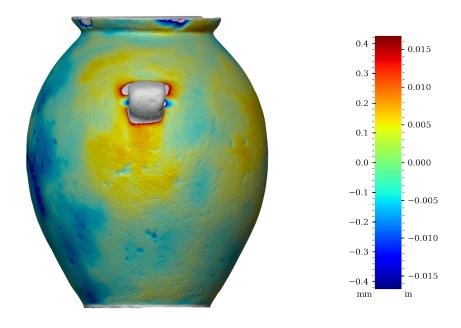


Figure 32: Surface variability heatmap of MV004, rotated 90°

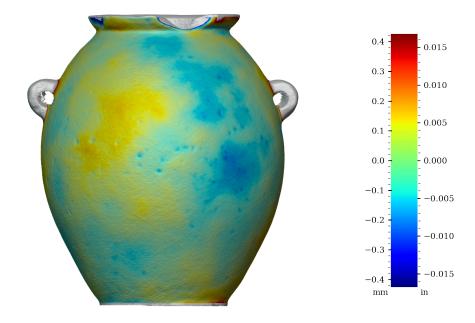


Figure 33: Surface variability heatmap of MV004, rotated 180 $^{\circ}$

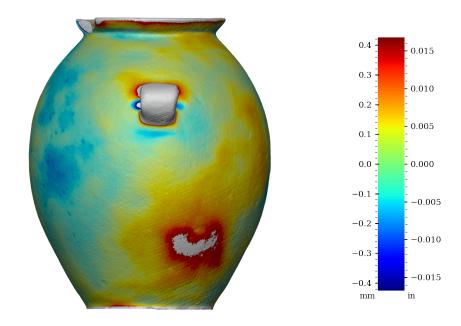


Figure 34: Surface variability heatmap of MV004, rotated 270°

Interior surface



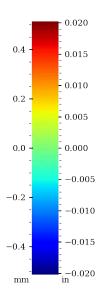


Figure 35: Surface variability heatmap of MV004, front view



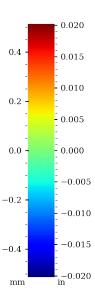


Figure 36: Surface variability heatmap of MV004, rotated 90°



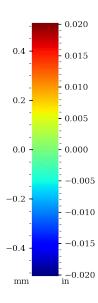
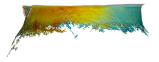


Figure 37: Surface variability heatmap of MV004, rotated 180°



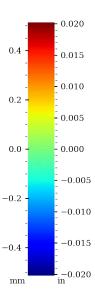


Figure 38: Surface variability heatmap of MV004, rotated 270°

Surface variability statistics

Area	MSD	RMSD	SD	Mean AD	Median AD	Range	Min	Max	Sample size
	mm^2	mm	mm	mm	mm	mm	mm	$_{ m mm}$	
Exterior	0.0148	0.122	0.122	0.082	0.096	0.928	-0.451	0.478	1597813
Interior	0.0295	0.172	0.172	0.107	0.144	1.351	-0.384	0.967	86325
	in^2	in	in	in	in	in	in	in	
Exterior	0.000023	0.0048	0.0048	0.0032	0.0038	0.0366	-0.0177	0.0188	1597813
Interior	0.000046	0.0068	0.0068	0.0042	0.0057	0.0532	-0.0151	0.0381	86325

Table 5: Surface variability statistics, MV004

Table 5 shows the statistics of the distance from the scan vertices to the best fit object model. These statistics are briefly explained below.

Mean Squared Deviation (MSD), also known as Mean Squared Error (MSE).

$$MSD = \frac{\sum_{i=1}^{n} (y_i - \hat{y})^2}{n}$$

The MSD metric shows the the average squared difference between the scanned points and the fitted composite polynomial model (a value of 0 would be a perfect match). This metric emphasizes imperfections in the surface of the artifact. Outliers will negatively influence this metric, raising the value of the MSE.

Root Mean Squared Deviation (RMSD), also known as Root Mean Squared Error (RMSE).

$$\text{RMSD} = \sqrt{\frac{\sum_{i=1}^{n} \left(y_i - \hat{y}\right)^2}{n}}$$

Measures the dispersion of the measured surface variability y_i around a model predictor (\hat{y}) . By obtaining the root of the MSD, the exponent will be removed from the measurement, enabling comparisons with other statistics of the same unit and making it more accessible to those familiar with the RMSD metric. This measure is used to assess the fit of a regression model to a dataset, in this case our best fit composite polynomial model. The lower the RMSD metric, the better the fit.

Standard Deviation (SD)

$$s = \sqrt{\frac{\sum_{i=1}^{n} \left(y_i - \bar{y}\right)^2}{n-1}}$$

Measures the dispersion of the measured surface variability y_i around the mean (\bar{y}) . If the residuals are normally distributed around the mean $(\bar{y}\approx 0)$, the SD will be equal to the RMSD. See Figure 39 and Figure 40

Mean Absolute Deviation (MeanAD)

$$\mathrm{MeanAD} = \frac{\sum_{i=1}^{n} \lvert y_i - \bar{y} \rvert}{n}$$

This metric is similar to the SD, but the difference between the residuals and the mean is *not* squared. Instead of indicating the spread of the data, we look at the average distance between each data point and the mean. The Mean Absolute Deviation is affected less by outliers than the Standard Deviation.

Median Absolute Deviation (MedianAD)

 $\operatorname{MedianAD} = \operatorname{median}(|y_i - \operatorname{median}(y)|)$

The Median Absolute Deviation is measure of the dispersion of the data around the median.

Range

$$\max(y_i) - \min(y_i)$$

Range is a measure of the total spread of the residuals

Histogram, KDE and Box-plot of measured surface variability - exterior surface

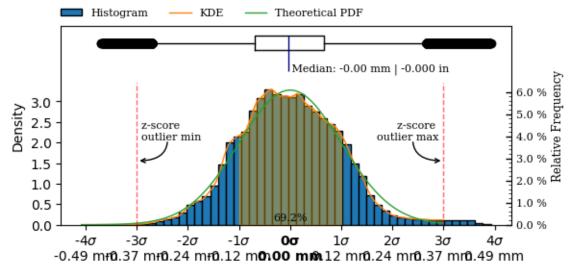


Figure 39: Exterior surface variability boxplot, kds and histogram.

Histogram, KDE and Box-plot of measured surface variability - interior surface

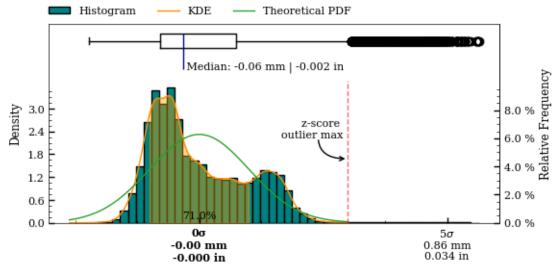


Figure 40: Interior surface variability boxplot, kds and histogram.

Precision Score Of The Artifact

To enable valid comparison of the manufacturing precision of different artifacts, a metric that robustly quantifies the overall precision of the object is required. The considerations for such a metric will be explored in this section.

Based on these considerations, a *Precision Score* metric will be defined.

For an object to be described as having been manufactured with high precision, several qualities must be present *concurrently*, and throughout the *entire* geometry of the final object. A given object may exhibit high levels of one or more *components* of precision, but be lacking in others. For example:

- An object may present high levels of coaxialility, but lack circularity.
- An object may exhibit good circularity, but show imperfections in the surface structure.
- An object may be smoothed to perfection *without* any circularity or coaxiality.
- An object may exhibit high levels of all of the above metrics in *some* areas, but not in others.

Therefore, a precision score metric **must** account for *all* aspects of the individual, underlying precision metrics (circularity, concentricity, coaxiality and surface variability) throughout the *entire* surface area of the object.

The composite high order polynomial model, used to generate the surface variability map (described in Surface Variability, p. 33) is the best continuous mathematical representation of the object available to us (lacking any original design plans, as would normally be available in metrological analysis). This idealized model encompasses all of the above component metrics.

In the creation of the model, all scan data-points are taken into account (excluding areas with extensive damage), making it the best possible idealized representation we can achieve. When this model has been accurately created, the deviation between the model and the scanned data-points can be calculated over the non-discretized polynomials, *without* the need for an "original" CAD model (and importantly, unless such a CAD model *actually* corresponded to the original design intent, it would be an insufficient comparison basis).

Within the context of defining a valid, overall precision metric, this approach satisfies the incorporation of all of the necessary metrics:

- **Circularity**: Because the reconstructed polynomial model is revolved around the Z-plane, the idealized representation is perfectly circular, and thus incorporates the circularity component.
- **Concentricity and coaxiality**: Because the Z-axis (datum axis) is the center axis of the model, it incorporates the concentricity and coaxiality components.
- **Surface variability**: Because the model is continuous and non-discretized, it can be used accurately for all points of the scan data, and incorporates the surface variability component.

The level of precision ultimately achieved in a physical object does not share a linear relationship with its manufacturing requirements. Since continuously higher levels of final precision becomes progressively harder to achieve, an overall precision metric must take this relationship into account.

A robust statistical metric that satisfies this requirement is the *Mean Squared Deviation* (MSD or MSE). Here specifically, we can utilize the mean square of the deviations between the model (\hat{y}) and the data-points (y_i) .

Combining all of the above considerations, we can express a well-defined *Precision Score* metric, that provides an immediately accessible way to understand the overall precision of an object, while being statistically valid. Since the Mean Squared Deviation tends towards zero as the overall precision increases, the inverse of the Mean Squared Deviation is taken to obtain a precision score metric that increases as precision increases¹²:

$$\text{Precision Score} = \frac{n}{\sum_{i=1}^{n} \left(y_i - \hat{y}\right)^2}$$

¹²The precision score unit is $\frac{1}{mm^2}$

A precision score will be calculated seperately for:

- The exterior surface
- The interior surface
- · The full surface

As most scans do not include sufficient scan data for the interior surface, the exterior surface will be used for calculating the precision score in most cases. In the rare case that the scan data is more complete for the *interior* surface, this will be used instead.

Table 6 shows the precision score of this artifact (MV004), compared to the two most precise, and the two least precise vessels currently analyzed.

Artifact		Material	Precision Score	Link to Report
	PV001	Red Granite	1905 Full: 980 Exterior: 1905 Interior: 705	Report Publication
	PV006	Dark grey granite	621 Full: 521 Exterior: 621 Interior: 152	Report Publication
The second secon	MV004	Basalt	68 Full: 64 Exterior: 68 Interior: 34	Report Publication
	MV001	Pottery	1.93 Full: 1.92 Exterior: 1.93 Interior: 1.85	Report Publication
18947 ©038	MV010	Calcite (Egyptian Alabaster)	Full: 0.64 Exterior: 1.12 Interior: 0.20	Report Publication

Analysis Roadmap

While the current iteration of this work already provides valuable results, continued future additions and improvements will enhance their utility further. This section details planned iterative updates and improvements, to both the reports themselves, and to the underlying methodology and software they are created with.

Alignment Section

- Detailed exploration of different circle regression algorithms
- If handles are present on the vessel, exploring alignment of the vessels so the handle positions match each other
- Add optimization of the perpendicular surface deviation, with the best results of the coaxial alignment
- Align by minimizing circularity results (of rotated sample slice, to compensate for sample height distortions)

Measurements of Precision

- Section detailing how measurements perpendicular to the surface curvature are obtained
- Detailed surface area analysis, exploring the residual patterns throughout subsequent sample slices of the artifact surface
- Wall thickness deviation color map
- Robust outlier identification on circularity, to better handle analysis of damaged areas of the artifacts in addition to removal of interior crystalline structure points present in CT scans
- · Layout updates to the charts and tables

Visibility of Outliers and Damaged Sections

- Identification and marking of damaged parts
- · Visualization of outliers on the artifact surface

Exploration of Mathematical Primitives

- Analysis of selected curvatures and flat surfaces on the vessel in both the horizontal and vertical planes
 - Circles
 - ▶ Parabolas
 - ► Ellipsoids
 - Hyperbolas
 - Cones
- Implementation of robust regressions models suitable for this domain, based on RANSAC.

Metrics on Primary Features

- Measurements of features in the horizontal plane
- Measurements of features in the vertical plane
- Measurements of angles
- Measurements of volume

Exploration of Potential Design Ratios

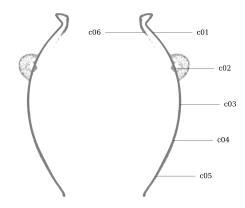
• π , φ , e, 1, 2, 3, 4 etc.

Raw Dataset Attachments

- Including all measurement and sample coordinates as CSV-files embedded in the report
- Including an STL file of the aligned object alongside the report, for easier external replication and validation of the research results

Appendix A - Comparison Of Circularity Measurements (Z-plane vs. surface-perpendicular)

Comparison of circularity samples



Samples perpendicular to the surface curvature

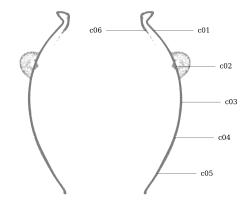
Tag	Area	Measured	Residuals	s			Sample	Slice		
		deviation ⁸	Range	RMSD ⁹	MAD ¹⁰	SD	size	Height	Z coord.	Radius ¹¹
		mm	mm	mm	mm	mm		mm	mm	mm
c01	exterior	Ø33.296±0.181	0.357	0.092	0.066	0.092	719	0.050	56.064	16.648
c02	exterior	Ø48.363±0.262	0.486	0.102	0.068	0.102	1102	0.050	43.831	24.182
c03	exterior	Ø51.991±0.343	0.594	0.139	0.110	0.139	1556	0.050	31.598	25.996
c04	exterior	Ø47.310±0.339	0.621	0.134	0.072	0.134	1328	0.050	19.365	23.655
c05	exterior	Ø35.338±0.292	0.497	0.120	0.080	0.120	912	0.050	7.133	17.669
c06	interior	Ø27.897±0.312	0.609	0.160	0.134	0.153	222	0.050	56.064	13.949

 $Table \ 7: Detailed \ circularity \ measurements \ at \ selected \ samples \ in \ z\text{-plane}, \ vessel \ MV004.$

Samples in the Z-plane

Tag	Area	Measured	Residuals	s			Sample	Slice		
		deviation ⁸	Range	RMSD ⁹	MAD^{10}	SD	size	Height	Z coord.	Radius ¹¹
		mm	mm	mm	mm	mm		mm	mm	mm
c01	exterior	Ø33.325±0.276	0.508	0.124	0.085	0.124	1280	0.050	56.064	16.662
c02	exterior	Ø48.394±0.307	0.531	0.109	0.073	0.109	1209	0.050	43.831	24.197
c03	exterior	Ø52.049±0.372	0.594	0.143	0.100	0.140	1541	0.050	31.598	26.025
c04	exterior	Ø47.263±0.379	0.651	0.140	0.067	0.139	1461	0.050	19.365	23.632
c05	exterior	Ø35.271±0.390	0.602	0.143	0.076	0.139	1203	0.050	7.133	17.635
c06	interior	Ø27.908±0.468	0.827	0.197	0.168	0.197	349	0.050	56.064	13.954

Table 8: Detailed circularity measurements at selected samples perpendicular to vessel curvature, vessel MV004.



Samples perpendicular to the surface curvature

Tag	Area	Measured	Residuals	s			Sample	Slice		
		deviation ⁸	Range	RMSD ⁹	MAD ¹⁰	SD	size	Height	Z coord.	Radius11
		in	in	in	in	in		in	in	in
c01	exterior	Ø1.3109±0.0071	0.0140	0.0036	0.0026	0.0036	719	0.0020	2.2072	0.6554
c02	exterior	Ø1.9041±0.0103	0.0191	0.0040	0.0027	0.0040	1102	0.0020	1.7256	0.9520
c03	exterior	Ø2.0469±0.0135	0.0234	0.0055	0.0043	0.0055	1556	0.0020	1.2440	1.0234
c04	exterior	Ø1.8626±0.0133	0.0245	0.0053	0.0028	0.0053	1328	0.0020	0.7624	0.9313
c05	exterior	Ø1.3912±0.0115	0.0196	0.0047	0.0032	0.0047	912	0.0020	0.2808	0.6956
c06	interior	Ø1.0983±0.0123	0.0240	0.0063	0.0053	0.0060	222	0.0020	2.2072	0.5492

Table 9: Detailed circularity measurements at selected samples in z-plane, vessel MV004.

Samples in the Z-plane

Tag	Area	Measured	Residual	s			Sample	Slice		
		deviation ⁸	Range	RMSD ⁹	MAD ¹⁰	SD	size	Height	Z coord.	Radius ¹¹
		in	in	in	in	in		in	in	in
c01	exterior	Ø1.3120±0.0109	0.0200	0.0049	0.0033	0.0049	1280	0.0020	2.2072	0.6560
c02	exterior	Ø1.9053±0.0121	0.0209	0.0043	0.0029	0.0043	1209	0.0020	1.7256	0.9526
c03	exterior	Ø2.0492±0.0146	0.0234	0.0056	0.0039	0.0055	1541	0.0020	1.2440	1.0246
c04	exterior	Ø1.8608±0.0149	0.0256	0.0055	0.0026	0.0055	1461	0.0020	0.7624	0.9304
c05	exterior	Ø1.3886±0.0154	0.0237	0.0056	0.0030	0.0055	1203	0.0020	0.2808	0.6943
c06	interior	Ø1.0987±0.0184	0.0326	0.0077	0.0066	0.0077	349	0.0020	2.2072	0.5494

 $Table\ 10: Detailed\ circularity\ measurements\ at\ selected\ samples\ perpendicular\ to\ vessel\ curvature,\ vessel\ MV004.$

Comparison of circularity on the full vessel surface

Metric

Samples perpendicular to the surface curvature

Area	Range			Standard	Deviation		Medan Al	bsolute De	Slices	Slice	
	Median Min. Max.			Median	Min.	Max.	Median	Min.	Max.		height
	$_{ m mm}$	$_{ m mm}$	$_{ m mm}$	mm	$_{ m mm}$		$_{ m mm}$				
Exterior	0.524	0.294	0.762	0.115	0.079	0.182	0.009	0.046	0.120	1194	0.050
Interior	0.706	0.470	1.284	0.168	0.099	0.233	0.010	0.057	0.205	124	0.050

 $Table \ 11: Detailed \ circularity \ measurements \ at \ selected \ samples \ in \ z\text{-plane}, \ vessel \ MV004.$

Samples in the z-plane

Area	Range			Standard	Standard Deviation			osolute De	Slices	Slice	
	Median	Min.	Max.	Median	Min.	Max.	Median	Min.	Max.		height
	$_{ m mm}$	$_{ m mm}$	$_{ m mm}$	mm	$_{ m mm}$	$_{ m mm}$	mm	$_{ m mm}$	$_{ m mm}$		mm
Exterior	0.572	0.357	0.866	0.129	0.092	0.197	0.009	0.050	0.130	1192	0.050
Interior	0.836	0.521	1.256	0.191	0.117	0.256	0.014	0.054	0.237	129	0.050

 $Table \ 12: Detailed \ circularity \ measurements \ at \ selected \ samples \ perpendicular \ to \ vessel \ curvature, \ vessel \ MV004.$

Imperial

Samples perpendicular to the surface curvature

Area	Range			Standard Deviation			Medan Al	osolute Dev	Slices	Slice	
	Median	Median Min. Max.			Min.	Max.	Median	Min.	Max.		height
	in	in	in	in	in	in	in	in	in		in
Exterior	0.524	0.294	0.762	0.115	0.079	0.182	0.009	0.046	0.120	1194	0.050
Interior	0.706	0.470	1.284	0.168	0.099	0.233	0.010	0.057	0.205	124	0.050

 $Table \ 13: Detailed \ circularity \ measurements \ at \ selected \ samples \ in \ z\text{-plane}, \ vessel \ MV004.$

Samples in the z-plane

Area	Range			Standard Deviation			Medan Al	osolute De	Slices	Slice	
	Median Min. Max.			Median	Min.	Max.	Median	Min.	Max.		height
	in	in	in	in	in	in	in	in	in		in
Exterior	0.572	0.357	0.866	0.129	0.092	0.197	0.009	0.050	0.130	1192	0.050
Interior	0.836	0.521	1.256	0.191	0.117	0.256	0.014	0.054	0.237	129	0.050

 $Table\ 14:\ Detailed\ circularity\ measurements\ at\ selected\ samples\ perpendicular\ to\ vessel\ curvature,\ vessel\ MV004.$

Circularity analysis of exterior samples perpendicular to surface curvature

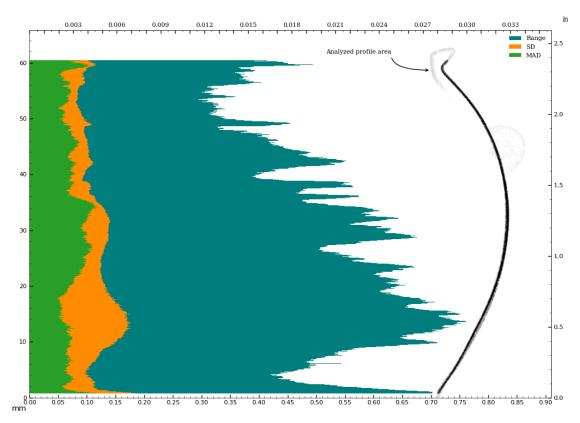


Figure 41: Circularity analysis of exterior samples perpendicular to surface curvature

Circularity analysis of exterior surface - in z-plane

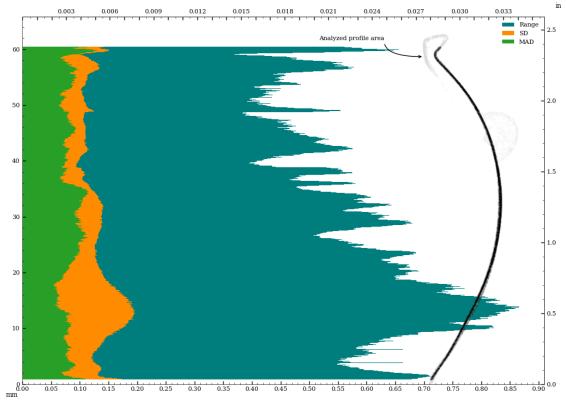


Figure 42: Circularity analysis of exterior surface - in z-plane

Circularity analysis of exterior samples perpendicular to surface curvature

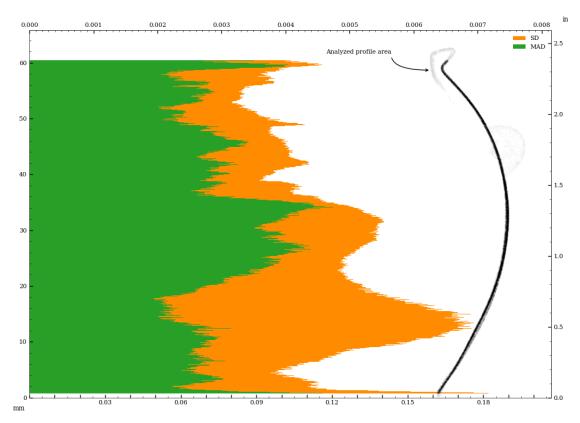


Figure 43: Circularity analysis of exterior samples perpendicular to surface curvature

Circularity analysis of exterior surface - in z-plane

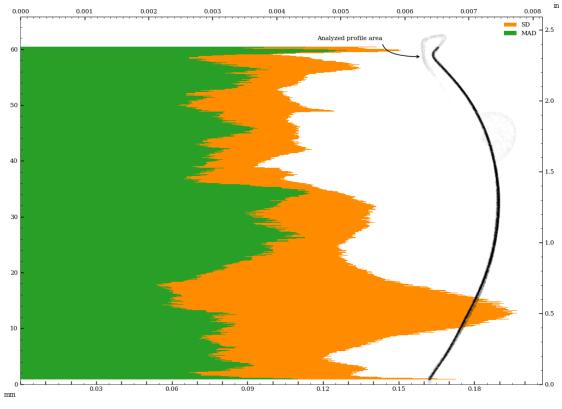


Figure 44: Circularity analysis of exterior surface - in z-plane

Circularity analysis of interior samples perpendicular to surface curvature

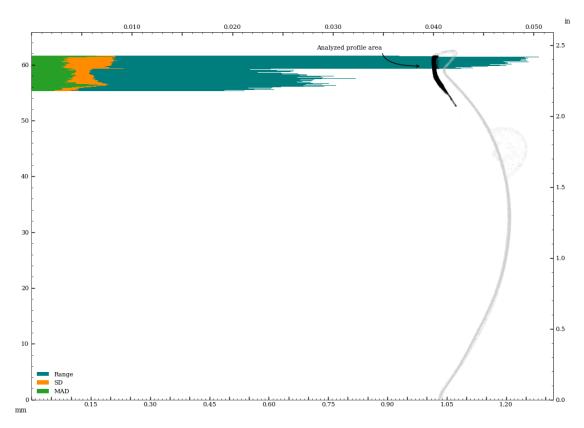


Figure 45: Circularity analysis of interior samples perpendicular to surface curvature

Circularity analysis of interior surface - in z-plane

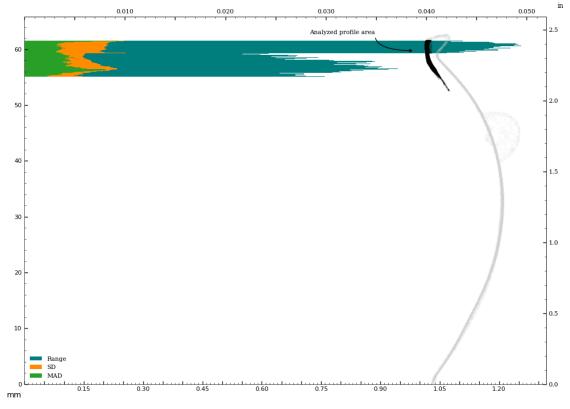


Figure 46: Circularity analysis of interior surface - in z-plane

Circularity analysis of interior samples perpendicular to surface curvature

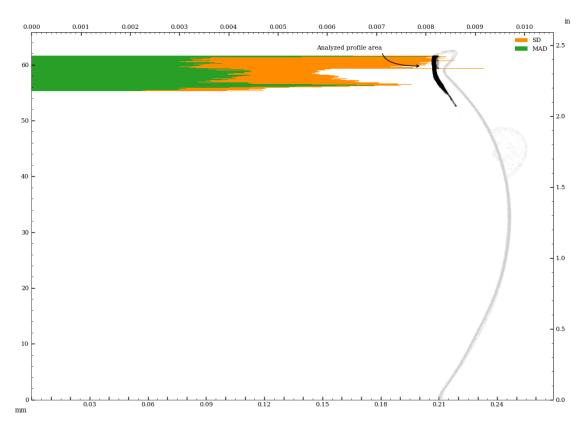


Figure 47: Circularity analysis of interior samples perpendicular to surface curvature

Circularity analysis of interior surface - in z-plane

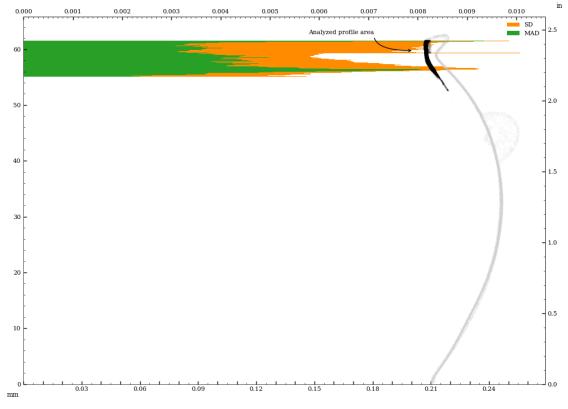


Figure 48: Circularity analysis of interior surface - in z-plane

Appendix B - Comparison Of Concentricity Measurements (Z-plane vs. surface-perpendicular)

 $\label{eq:Metric} Metric \\ \textbf{Concentricity measurements perpendicular to surface curvature}$

Tag	Reference	Deviation	Sample	Circle fit	residuals an	alysis for sa	mple listed	in Tag colu	mn	
			size	Range full	Range inliers	SD full	SD inliers	MAD full	MAD inliers	Center (x,y)
		$_{ m mm}$		$_{ m mm}$	$_{ m mm}$	$_{ m mm}$	$_{ m mm}$	$_{ m mm}$	$_{ m mm}$	$\mu \mathrm{m}$
c01	z-axis	0.046	706	0.357	0.357	0.093	0.093	0.062	0.062	-38, -26
c02	z-axis	0.018	1102	0.486	0.486	0.102	0.101	0.069	0.069	12, 13
c03	z-axis	0.020	1556	0.594	0.594	0.139	0.139	0.101	0.101	20, 1
c04	z-axis	0.095	1328	0.621	0.621	0.134	0.134	0.066	0.066	-95, 12
c05	z-axis	0.111	912	0.497	0.497	0.120	0.120	0.074	0.074	-110, 8
c06	z-axis	0.203	222	0.609	0.609	0.153	0.153	0.121	0.121	-202, 17
c01	c06	0.170	706	0.357	0.357	0.093	0.093	0.062	0.062	165, -43

Concentricity measurements in z-plane

Tag	Reference	Deviation	Sample	Circle fit	residuals an	alysis for sa	mple listed	in Tag colu	mn	
			size	Range full	Range inliers	SD full	SD inliers	MAD full	MAD inliers	Center (x,y)
		$_{ m mm}$		$_{ m mm}$	$_{ m mm}$	$_{ m mm}$	$_{ m mm}$	$_{ m mm}$	$_{ m mm}$	$\mu \mathrm{m}$
c01	z-axis	0.087	1280	0.615	0.615	0.154	0.153	0.104	0.103	-71, -50
c02	z-axis	0.017	1209	0.521	0.499	0.111	0.109	0.079	0.079	10, 13
c03	z-axis	0.024	1541	0.595	0.595	0.139	0.139	0.099	0.099	24, -2
c04	z-axis	0.104	1461	0.638	0.638	0.135	0.135	0.075	0.075	-102, 18
c05	z-axis	0.145	1203	0.600	0.600	0.138	0.138	0.076	0.076	-145, 2
c06	z-axis	0.332	349	0.790	0.790	0.195	0.192	0.163	0.158	-331, 21
c01	c06	0.270	1280	0.615	0.615	0.154	0.153	0.104	0.103	261, -71

 ${\bf Imperial}$ ${\bf Concentricity\ measurements\ perpendicular\ to\ surface\ curvature}$

Tag	Reference	Deviation	Sample	Circle fit	mn					
			size	Range full	Range inliers	SD full	SD inliers	MAD full	MAD inliers	Center (x,y)
		in		in	in	in	in	in	in	thou
c01	z-axis	0.0018	706	0.0140	0.0140	0.0037	0.0037	0.0024	0.0024	-1.5, -1.0
c02	z-axis	0.0007	1102	0.0191	0.0191	0.0040	0.0040	0.0027	0.0027	0.5, 0.5
c03	z-axis	0.0008	1556	0.0234	0.0234	0.0055	0.0055	0.0040	0.0040	0.8, 0.0
c04	z-axis	0.0038	1328	0.0245	0.0245	0.0053	0.0053	0.0026	0.0026	-3.7, 0.5
c05	z-axis	0.0044	912	0.0196	0.0196	0.0047	0.0047	0.0029	0.0029	-4.3, 0.3
c06	z-axis	0.0080	222	0.0240	0.0240	0.0060	0.0060	0.0048	0.0048	-8.0, 0.7
c01	c06	0.0067	706	0.0140	0.0140	0.0037	0.0037	0.0024	0.0024	6.5, -1.7

Concentricity measurements in z-plane

Tag	Reference	Deviation	Sample	Circle fit residuals analysis for sample listed in Tag column						
			size	Range full	Range inliers	SD full	SD inliers	MAD full	MAD inliers	Center (x,y)
		in		in	in	in	in	in	in	thou
c01	z-axis	0.0034	1280	0.0242	0.0242	0.0060	0.0060	0.0041	0.0041	-2.8, -2.0
c02	z-axis	0.0007	1209	0.0205	0.0197	0.0044	0.0043	0.0031	0.0031	0.4, 0.5
c03	z-axis	0.0009	1541	0.0234	0.0234	0.0055	0.0055	0.0039	0.0039	0.9, -0.1
c04	z-axis	0.0041	1461	0.0251	0.0251	0.0053	0.0053	0.0029	0.0029	-4.0, 0.7
c05	z-axis	0.0057	1203	0.0236	0.0236	0.0054	0.0054	0.0030	0.0030	-5.7, 0.1
c06	z-axis	0.0131	349	0.0311	0.0311	0.0077	0.0076	0.0064	0.0062	-13.0, 0.8
c01	c06	0.0106	1280	0.0242	0.0242	0.0060	0.0060	0.0041	0.0041	10.3, -2.8